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(94) Can end shells.

(57) Apparatus for forming a reinforced pressure resistant can end shell from sheet material comprises a cutting ring (11), a cutting punch shell (13) enterable into said ring (11) to blank out a disc of material therebetween, an annular draw ring (14) axially aligned with said cutting punch shell (13) to support a peripheral margin of the disc held against it by said cutting punch shell, a die centre ring (15) arranged coaxially and slidably within the draw ring (14) and having an end face profiled to define a surface of a seaming panel of the can end shell, an ejector pressure ring (19) arranged coaxially and slidably within the punch shell and axially aligned with the die centre ring so that when in use peripheral material of the blank is restrained between the die centre ring and the ejector pressure ring, a draw punch centre (16) arranged coaxially and slidably within the ejector pressure ring and a reform pad (20) arranged coaxially and slidably within the die centre ring to engage the central panel of the blank opposite the draw punch centre. The end profile of the punch centre comprises an annular radiused nose (22) surrounding and defining a central substantially frustoconical recess (23), and the reform pad comprises a central cylindrical portion, dimensioned to deform the central portion of the blank around the nose (22) of the punch centre and into the recess (23), and an outer ring (31) spaced from

the central cylindrical portion by an annular recess (30) dimensioned to receive the nose of the punch centre; the outer ring having an inward facing substantially frustoconical face (311) which flares outwards from the recess (30).

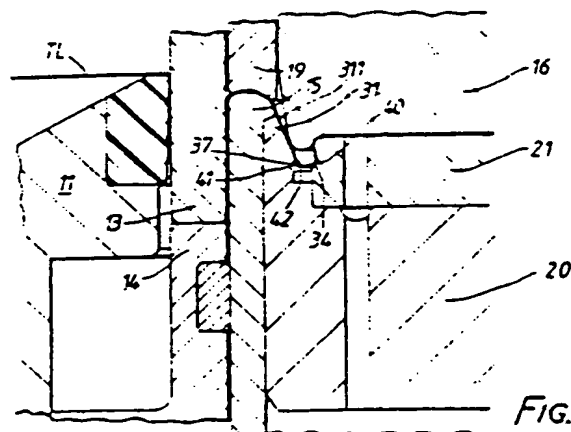


Fig. 10.

EP 0 340 955 A1

## CAN END SHELLS

The invention relates to the production of can end shells for seaming onto the ends of can bodies to form cans capable of withstanding substantial internal pressures.

The can end shells to which the invention relates comprise an annular flange or seaming panel for seaming the shell to a can body, a frustoconical chuck wall, a flat central panel, and an annular, generally U-shaped, channel known as an anti-peaking bead connecting the chuck wall to the central panel. Apparatus for making can end shells of this type is described for example in US 3537291, US 3957005, US 4109599, and EP 0153115. In US 3537291 and US 3957005, the anti-peaking bead is formed by a profiled punch acting against a fixed correspondingly profiled die. In US 4109599 a preliminary shell comprising a peripheral seaming panel, a frustoconical wall and a flat central panel is formed in a first stage and, in a second stage, the central panel is moved towards the seaming panel such that a reinforcing anti-peaking bead is formed between the frustoconical wall and the central panel. The anti-peaking bead is formed largely by bending and is constituted by material from the outer periphery of the central panel of the preliminary shell. In EP 0153115 the two stages described in relation to 4109599 are carried out sequentially in a single piece of apparatus. In this case however the anti-peaking bead is formed by a reforming action which incorporates material from the frustoconical wall into the anti-peaking bead.

It is known that the resistance of a can end shell to internal pressures after seaming onto a can body is dependent upon the profile of the anti-peaking bead and thickness of the material from which the shell is made. The art of making can end shells, without tightening (reforming) of the anti-peaking bead, permitted use of aluminium sheet 0.32 mm thick for a can end of about 57 mm diameter ("206"). The combined shell drawing and reforming apparatus described in EP-0153115 permitted use of aluminium alloy sheet 0.29 mm thick with a possibility of using sheet 0.27 mm thick. In order to make can end shells from lower nominal gauge material it is desirable to make the nominal radius of the anti-peaking as small as possible whilst avoiding the creation of overworked areas in the anti-peaking bead leading to yield of material and failure under pressure.

The present invention relates to an improved method and apparatus for making can end shells from thin gauge stock material (such as aluminium alloy sheet in the range 0.245 to 0.29 mm thick) and having anti-peaking beads of small nominal

radius and in which the creation of overworked regions in the anti-peaking bead are avoided.

Accordingly the present invention provides for making a preliminary shell in which a preformed anti-peaking bead in the form of a generally U-shaped channel having a relatively large nominal radius is formed in a controlled drawing action by means of corresponding profiles on a punch centre, a die, and a reform pad. In a second stage, material from the frustoconical wall is reformed into the anti-peaking bead whilst being urged radially inwardly to form a final shell having an anti-peaking bead of relatively narrow nominal radius.

According to a first aspect of the present invention there is provided apparatus for forming a reinforced pressure resistant can end shell from sheet material, said apparatus comprising a cutting ring, a cutting punch shell enterable into said ring to blank out a disc of material therebetween, an annular draw ring axially aligned with said cutting punch shell to support a peripheral margin of the disc held against it by said cutting punch shell, a die centre ring arranged coaxially and slidably within the draw ring and having an end face profiled to define a surface of a seaming panel of the can end shell, an ejector pressure ring arranged coaxially and slidably within the cutting punch shell and axially aligned with the die centre ring so that when in use peripheral material of the blank is restrained between the die centre ring and the ejector pressure ring, a draw punch centre arranged coaxially and slidably within the ejector pressure ring and a reform pad arranged coaxially and slidably within the die centre ring to engage the central panel of the blank opposite the draw punch centre; wherein the end profile of the draw punch centre comprises an annular radiused nose surrounding and defining a central substantially frustoconical recess, and the reform pad comprises a central cylindrical portion, dimensioned to deform the central portion of the blank around the nose of the punch centre and into the recess, and an outer ring spaced from the central cylindrical portion by an annular recess dimensioned to receive the nose of the punch centre; the outer ring having an inward facing substantially frustoconical face which flares outwardly from the recess.

The invention also provides a method of forming a reinforced pressure-resistant can end comprising the steps of providing a substantially planar metallic blank having a central portion and a peripheral portion, deforming the blank in a first deformation stage to cause movement apart of the central and peripheral portions to offset said portions out of a common plane, thus drawing the

blank into a generally flanged cup-shaped configuration defined by the central portion, a generally U-shaped channel, a frustoconical wall and an annular seaming panel, and, in a second deformation stage, causing movement towards one another of the central portion and annular seaming panel to deform at least a part of the metal of the frustoconical wall into the U-shaped channel to form an anti-peaking bead of the can end shell; wherein, during the second stage, the frustoconical wall is progressively pushed radially inwardly.

The invention also provides can end shells having a particular desired profile.

A detailed description of the present invention is provided below with reference to the accompanying drawings in which:-

FIGURES 1-15 are partial views of apparatus for forming can end shells shown at different stages of operation;

FIGURES 16 and 17 are overall views of two embodiments of apparatus for forming can end shells;

FIGURE 18 shows a section through part of a finished can end shell; and

FIGURES 19-21 are partial views of a modified apparatus.

Figure 1 shows a sheet TL of aluminium alloy or steel stock which has been fed by a standard mechanism to be positioned above the die of a double action press tool such as that shown in more detail in Figures 16 and 17. As shown in Figure 1 the sheet stock is positioned immediately above the cutting ring 11 having a cutting edge 12. The punch plate 1 (See Figures 16 and 17) along with parts carried thereon is driven directly by the ram of the press and has descended to the point where the leading component of the punch assembly, the cutting punch shell 13, is just about to clamp the stock against an annular draw ring 14 which is resiliently supported on the die assembly such as by pneumatic (as shown), hydraulic or nitrogen pressure or by springs. As the punch assembly continues to descend a circular blank is cut by the cutting edges of the punch shell 13 and the cutting ring 11. The periphery of the blank is supported between opposed faces of the punch shell 13 and the draw ring 14 as the punch assembly continues to descend. When the die centre ring 15 engages the blank, continuing descent of the punch deforms the periphery of the blank downwardly.

As shown in Figure 2 the outer periphery of the blank is drawn radially inwardly between the punch shell 13 and draw ring 14 which provide sufficient pressure to prevent wrinkling. The periphery is also drawn around a draw radius at the juncture of the leading and inner faces of the punch shell. Thus

the blank is formed into an inverted cup known as a reverse cup. The cup may have a flanged edge: the ratio of cup depth to flange width being dependent upon punch shell profile and press selection. The flange width is also dependent on the length of the punch shell such that a new punch shell may produce no flange whereas a re-ground punch shell may produce a slight flange.

Figure 3 shows the punch assembly's continued progress downwardly. Directly after the stage shown in Figure 2, the punch centre 16 starts to penetrate the horizontal plane of the central portion of the reverse cup, thus deforming it in a downward direction and drawing it around an inner radius on the die centre ring 15, drawing it downwardly and inwardly to form a generally frustoconical wall 17 and a flat central portion 18 having a juncture of a radius determined by the punch centre profile. Shortly after the downward central deformation begins, the ejector pressure ring 19 makes contact with the blank opposite the upper portion of the die centre ring known as the seaming panel portion. The ejector pressure ring 19 has a concave profile complementary to the profile of the seaming panel portion of the die centre ring 15 but with each radius increased by the nominal material gauge. Thus the pressure exerted by the ring 19 provides a restraining force to the portion of the blank which is drawn from the flange of the reverse cup over the convex portion of the die centre ring and thus prevents wrinkling.

Figure 4 shows the punch centre 16 and punch shell 13 continuing to descend to the point where the flat centre 18 of the blank is engaged by the reform pad 20 and is deformed in a controlled fold over the nose 21 of the reform pad and around the nose 22 of the punch centre into a substantially frustoconical recess 23 in the lower face of the punch centre. The reform pad 20 is resiliently (e.g. pneumatically) supported on the die assembly and from this point onwards the central panel 18 of the blank is clamped between the punch centre 16 and the reform pad 20.

During further descent of the punch centre as shown in Figures 5, 6 and 7, the reform pad moves downwardly relative to the die centre ring and further metal is drawn from the wall of the reverse cup which is progressively sacrificed to provide a deeper frustoconical wall 17. At the point shown in Figure 7 the ram driving the punch centre 16 has reached bottom dead centre, the outer edge of the blank has reached its final height, known as the start curl height, and the frustoconical wall 17 has reached its greatest depth.

At this stage a preliminary can end shell has been formed and comprises a seaming panel and start curl portion 25, a frustoconical chuck wall 26, a flat central panel 18 and a generally U-shaped

channel 27 which is the preliminary form of an anti-peaking bead.

As the ram passes its bottom dead centre position it begins to ascend as shown in Figures 8 and 9 carrying the punch centre 16 and punch shell 13 upwardly. The ring 19 continues, however, to exert pressure over the seaming panel portion of the shell; the energy required being stored during the downward stroke of the ram.

Energy stored by the reform pad 20 during its downward motion causes this to follow the punch centre 16 on its ascent and to exert an upward force on the central panel 18 of the can end shell to re-form the shell as described below. This force is, however, not sufficient to overcome the force applied to the seaming panel by the ring 19 so metal is not pushed back out between the die centre ring 15 and the ring 19 during re-forming and the start curl and seaming panel portion 25 of the shell can therefore be considered to be isolated from the effects of the re-forming action.

The upward force exerted by the reform pad 20 is sufficient to overcome the mechanical strength of the shell which is thus deformed as shown in Figures 8, 9 and 10.

As can be seen from the drawings, the reform pad comprises a central portion or nose 21 surrounded by an annular recess 30 and an outer annular ring portion 31 which has a frustoconical face 311 flaring outwardly from the recess at an angle B to the axis of the apparatus; the chuck wall 26 being inclined at an angle A when the ram is at B.D.C. (Figure 7), and angle B being greater than angle A. Thus as the reform pad rises, the outer ring 31 thereof engages the chuck wall 26 and progressively deforms it radially inwardly. This action pushes the material of the wall 26 into the anti-peaking bead 27 while the relative upward motion of reform pad nose 21 cooperates to tighten the "fold" of the channel 27.

The die centre ring 15 has a re-entrant surface which forms an axial abutment for the outer ring 31 in its fully raised position (Figure 10) where the frustoconical face 311 and the seaming panel portion of the die centre ring form a substantially smooth continuous surface.

The nose 21 of the reform pad is formed with a radiused profile which accommodates the transition from the plane of the end face 28 of the reform pad which engages the central panel 18 to the generally cylindrical wall 29 of the nose 21 of the reform pad which engages the radially inner panel wall 34 of the anti-peaking bead. Immediately below the centre line of this radius the nose is formed with a generally V-shaped undercut 32 which has an upper face 33 lying tangential to the nose radius. The undercut 32 provides increased clearance between the nose 21 of the reform pad and

its outer ring 31 thus allowing the formation of a relatively large radius at the junction of the chuck wall and the anti-peaking bead and avoiding the creation of a critically tight radius at this point and the consequent creation of a highly strained weakened area of the shell after the material of this point has moved through the anti-peaking bead during the re-forming stage to the inner substantially cylindrical panel wall 34 of the anti-peaking bead.

Figure 9 shows the tooling approaching the fully reformed position. Here it can be seen that the bead 27 at this stage comprises several radii; the two most important being the radius 35 at the chuck wall juncture and the radius 36 at the juncture with the panel wall 34. It is known that the nominal radius of the anti-peaking bead is related to the peaking pressure of the shell when seamed onto a can and subjected to internal pressure. It can be observed that in these circumstances the centre panel 18 acts as a diaphragm which is deflected outwardly (upwards as viewed in the drawings). The result of this deflection of the central panel is to place the panel wall 34 and its radius 36 with the bottom of the anti-peaking bead under tensile force which tries to unwind the anti-peaking bead. It can be shown that the main resistance to unwinding is provided by the material of the radius 35 supported by the chuck wall. The anti-peaking bead transfers tensile force in the central panel to compressive force in the chuck wall.

It follows that the provision of an anti-peaking bead having an outer radius 35 tighter than the inner radius 36 but with the nominal width of the channel forming the bead unchanged, will increase pressure resistance.

Figure 9 shows the anti-peaking bead shortly before the end of the reforming action having a large outer radius 35 and a smaller inner radius 36 - i.e. the opposite of the desired profile. It can also be seen, however, that as the panel wall 34 extends progressively into the recess 30 it contacts the lower conical face 40 of the undercut 32 which slopes downwardly and outwardly.

From Figure 10 it can be seen that the influence of the face 40 has been to urge the panel wall 34 outwardly to become substantially cylindrical. Further it can be seen that the outer ring 31 of the reform pad is formed with an undercut 41 at the lower end of the face 311 and directly opposite the flank angle of the face 40. The undercut 41 leads to the creation of an annular convex kink 42 in the shell; being a work hardened region at the lower end of the generally conical chuck wall which resists deformation of the chuck wall when the shell is subjected to internal pressure. At the point just below the kink 42 a tight radius 37 is formed.

It will be seen that in the final form of the shell

as shown in Figure 10, the required differential between the inner and outer radii of the anti-peaking bead has been achieved and that the nominal radius of the anti-peaking bead is smaller than that of the U-shaped channel 27 as formed in the preliminary shell (Figure 7). More specifically the can end shown in Figure 10 has a peripheral flange ready for a final curling operation; a frustoconical wall extending axially and inwardly from the interior of the peripheral flange; an anti-peaking bead including an annular kink portion 42 and a radiused portion which extend from the frustoconical wall to join an annular panel wall 34 which extends in a substantially axial direction to support a flat central panel 18.

The removal of the completed shell from the apparatus is shown in Figures 11-15. Figure 11 shows the tooling in ascendance immediately after the completion of the reforming action. At this point the reform pad 20 has reached its uppermost position and the centre panel 18 is no longer clamped, but the seaming panel of the shell is still clamped against the die centre ring 15 by the ejector pressure ring 19.

Further ascent of the punch tooling is shown in Figure 12 where the ejector pressure ring 19 has lifted away from the die centre ring 15 and resilient expansion of the shell causes it to be held within the bore of the punch shell 13 as it is raised.

Figure 13 shows the punch tooling at top dead centre where the ejector pressure ring is actuated by a timed cam and follower to strip the shell from the bore of the punch shell. A timed kicker 50 operates to knock the shell clear of the tooling in known manner.

Figures 14 and 15 show alternative means for supporting the blank at the start and ejecting the shell at the end of the shell forming cycle respectively.

In this alternative the length of the ejector pressure ring 19 is increased and the ring 19 now applies pressure to the seaming panel portion of the shell through most of the forming action and strips the shell from the bore of the punch shell without the need for cam actuation at T.D.C. This leaves the shell in the die and a lift ring 60 is provided to lift the shell out of the die tooling as shown in Figure 15. The lift ring 60 may be fluidically supported as shown or may for example be operated by a timed cam mechanism. The shell is finally removed from the tooling by conventional means such as a kicker or an air blast indicated by arrows in Figure 15.

Figures 16 and 17 show in greater detail the overall arrangement of embodiments of the apparatus. The apparatus of Figure 16 is modified from that described in European Patent Application no. 0153115 to which reference is made for a more

detailed description of the overall construction and operation of the apparatus. In both Figures 16 and 17 the apparatus is shown at bottom dead centre.

The main components of the apparatus of Figures 16 and 17 which have not been referenced in the other drawings are as follows: punch plate 1, punch body 2, press bolster 3, lower pressure assembly 4, upper pressure assembly 5, stripper 6 and retainer 7.

Figure 18 shows a partial section through a finished can end shell having been released from the apparatus. In the example, a can end shell has been made from 0.245 mm thick aluminium alloy 5182 in H19 temper. The thickness  $t$  of the central panel 18 is the same as the thickness of the sheet stock. The frustoconical chuck wall 26 is inclined to the axis of the shell at an angle  $C$  which is preferred to be in the range from  $12^\circ$  to  $20^\circ$  and more preferably in the range from  $12^\circ$  to  $15^\circ$ . The angle  $D$  representing the angle of the anti-peaking bead below the kink 42 is preferred to be in the range of  $2^\circ$  to  $10^\circ$  and more preferably is in the range of  $2^\circ$  to  $4^\circ$ . The angle  $E$  represents the inclination of inner panel wall 34 to the axis. The panel wall 34 is preferred to be parallel to the axis of the shell but may incline in either direction by up to  $5^\circ$ . A first annular portion 35 of the anti-peaking bead at its juncture with the panel wall has a radius of curvature  $R$  which is preferred to be in the range from .18 mm to 0.5 mm. A second annular portion 36 of the anti-peaking bead at its juncture with the chuck wall 26 below the kink 42 has a radius of curvature  $r$  which is preferred to be in the range from .18 mm to .43 mm.

An annulus 38 joins the first annular portion 35 to the second annular portion 36. Whilst we think it is preferable that  $R$  be greater than  $r$ , useful can ends may have  $R$  equal to  $r$  or  $R$  less than  $r$ . The centres of the radiuses  $R$  and  $r$  are spaced by a distance  $L$ .

The apparatus described above permits considerable control of the shape of the anti-peaking bead by choice of dimensions and adjustment of the travel of reform pad 21 to control how much of the frustoconical wall is transferred into the anti-peaking bead by entry into the recess 30, the width of which governs the width of anti-peaking bead created. A short travel will not create a kink 42: a longer travel will fill the "v" shaped undercut 32 and recess 30 to control the radii  $R, r$ .

Figures 19 to 21 show a modification of the apparatus in which the frustoconical surface 311 has been replaced by a gentle convex arc 312, the curvature of which acts as a cam to time the rate of movement of chuck wall material into the evolving anti-peaking bead so that further control of the shape of the anti-peaking bead is achieved.

The apparatus shown in Figures 19 and 20 has

many parts identical to those already described with reference to Figures 1 to 15 so that like functioning parts are denoted by the same integer numbers; such as the pressure sleeve 19 and punch centre 16 of the top tool, and die centre ring 15 of the bottom tool. However, in Figure 19, it will be seen that the outer annular ring portion 31 of the reform pad has a gentle convex arcuate surface 312, best seen in Figure 20. At bottom dead centre, as shown in Figure 19, drawing of the preliminary can end shell is complete and the chuck wall extends as a frustum of a cone clear of both the side wall of punch centre 16 and the convex arc 312 which has been pushed down by the punch centre 16 acting through the sheet metal on the nose 21 of the reform pad.

Figure 21 shows the apparatus of Figure 19 at the end of the reforming operation, the outer ring portion 31 has risen to abut the beak of the die centre ring 15 and, in so doing, has progressively pushed chuck wall material into the anti-peaking bead at a rate and a distance governed by the convex arc 312. In the manufacture of a can end of diameter 57 mm from aluminium alloy sheet 0.45 mm thick the convex arc has typically a radius R, of about 75 mm and extends a vertical distance of about 3.8 mm as shown on an enlarged scale in Figure 20.

Choice of suitable dimensions for gentle convex arc therefore provides a means to localised modification of the shape of the anti-peaking bead. The lateral thrust delivered by the convex arc 312 or the frustoconical surface 311 may cause some advantageous thickening of the material of the anti-peaking bead.

In the embodiment of Figures 19-21 the nose 21 of the reform pad has a smoother profile; the V-shaped undercut 32 being omitted from this embodiment.

## Claims

1. Apparatus for forming a reinforced pressure resistant can end shell from sheet material, said apparatus comprising a cutting ring (11), a cutting punch shell (13) enterable into said ring (11) to blank out a disc of material therebetween, an annular draw ring (14) axially aligned with said cutting punch shell (13) to support a peripheral margin of the disc held against it by said cutting punch shell, a die centre ring (15) arranged coaxially and slidably within the draw ring (14) and having an end face profiled to define a surface of a seaming panel of the can end shell, an ejector pressure ring (19) arranged coaxially and slidably within the cutting punch shell and axially aligned with the die centre ring so that when in use peripheral material of the

blank is restrained between the die centre ring and the ejector pressure ring, a draw punch centre (16) arranged coaxially and slidably within the ejector pressure ring and a reform pad (20) arranged coaxially and slidably within the die centre ring to engage the central panel of the blank opposite the draw punch centre; wherein the end profile of the draw punch centre comprises an annular radiused nose (22) surrounding and defining a central substantially frustoconical recess (23), and the reform pad comprises a central cylindrical portion, dimensioned to deform the central portion of the blank around the nose (22) of the punch centre and into the recess (23), and an outer ring (31) spaced from the central cylindrical portion by an annular recess (30) dimensioned to receive the nose of the punch centre; the outer ring having an inward facing substantially frustoconical face (311;312) which flares outwardly from the recess (30).

2. Apparatus according to claim 1 wherein the radially inner wall of the annular recess (30) is provided by a generally cylindrical wall (29) of the central cylindrical portion (21) of the reform pad, and is formed with an annular generally V-shaped undercut (32).

3. Apparatus according to claim 1 or claim 2 wherein the radially outer wall of the annular recess (30) is provided by a generally cylindrical wall of the outer ring (31) and is formed with an annular undercut (41) at its juncture with the frustoconical wall (311;312).

4. Apparatus according to any one of claims 1-3 wherein the die centre ring (15) has a re-entrant surface which forms an axial abutment for the outer ring (31) in its fully raised position and wherein the frustoconical face (311;312) of the outer ring (31) and the seaming panel portion of the die centre ring form a substantially smoothly continuous surface when the die centre ring (15) and the outer ring (31) are in axial abutment.

5. A method of forming a reinforced pressure-resistant can end comprising the steps of providing a substantially planar metallic blank having a central portion and a peripheral portion, deforming the blank in a first deformation stage to cause movement apart of the central and peripheral portions to offset said portions out of a common plane, thus drawing the blank into a generally flanged cup-shaped configuration defined by the central portion, a generally U-shaped channel, a frustoconical wall and an annular seaming panel, and, in a second deformation stage, causing movement towards one another of the central portion and annular seaming panel to deform at least a part of the metal of the frustoconical wall into the U-shaped channel to form an anti-peaking bead of the can end shell; wherein, during the second stage, the frustoconical wall is progressively pushed radially inwardly.

6. A can end comprising a peripheral seaming panel (25), a frustoconical wall (26) depending from the inner periphery of the peripheral seaming panel, a generally "U" shaped anti-peaking bead extending radially inward from the frustoconical wall, an annular wall extending in an axial direction from the inner periphery of the anti-peaking bead, and a generally flat central panel supported within the frustoconical wall by said annular wall, characterized in that the anti-peaking bead comprises a first annular portion 35 of arcuate cross-section extending outwards from the annular wall 34, a second annular portion 36 of arcuate cross-section extending inwards from a substantially frustoconical chuck wall 26, and an annular connecting portion 38 joining said first annular portion to said second annular portion.

7. A can end according to claim 6 wherein the radius of curvature  $R$  of the first annular portion is greater than the radius of curvature of the second annular portion.

8. A can end according to claim 6 wherein the radius of curvature  $R$  of the first annular portion 35 is less than the radius of curvature  $r$  of the second annular portion 36.

9. A can end according to any one of claims 6 to 8 wherein the frustoconical chuck wall includes a kink 42 joining the second annular portion 36 to the chuck wall 26.

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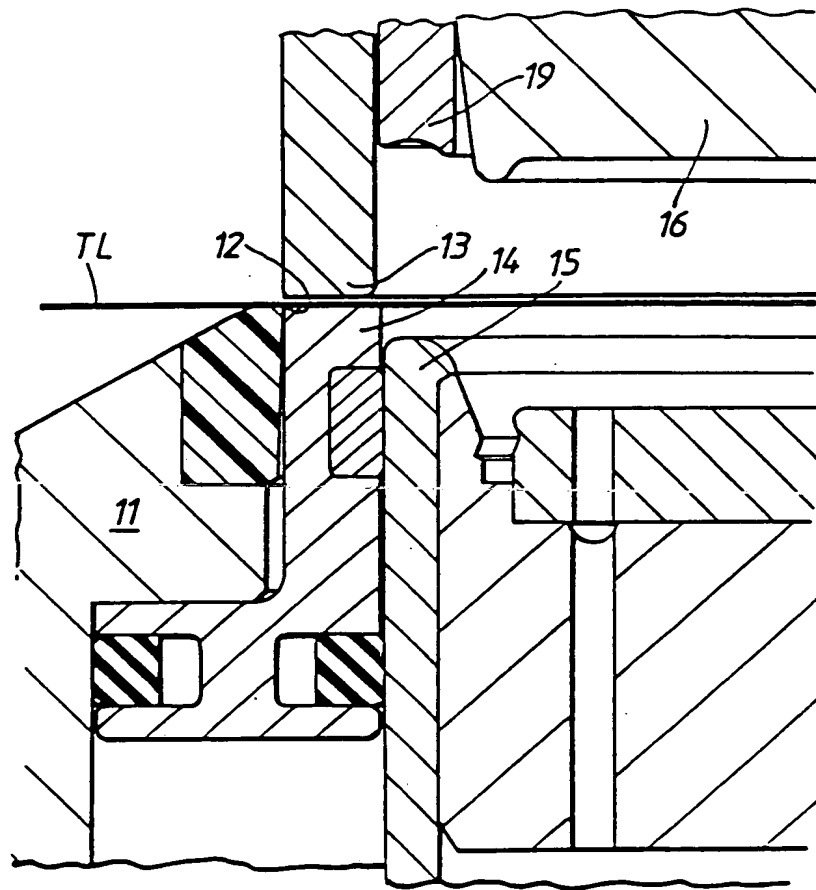


FIG. 1.

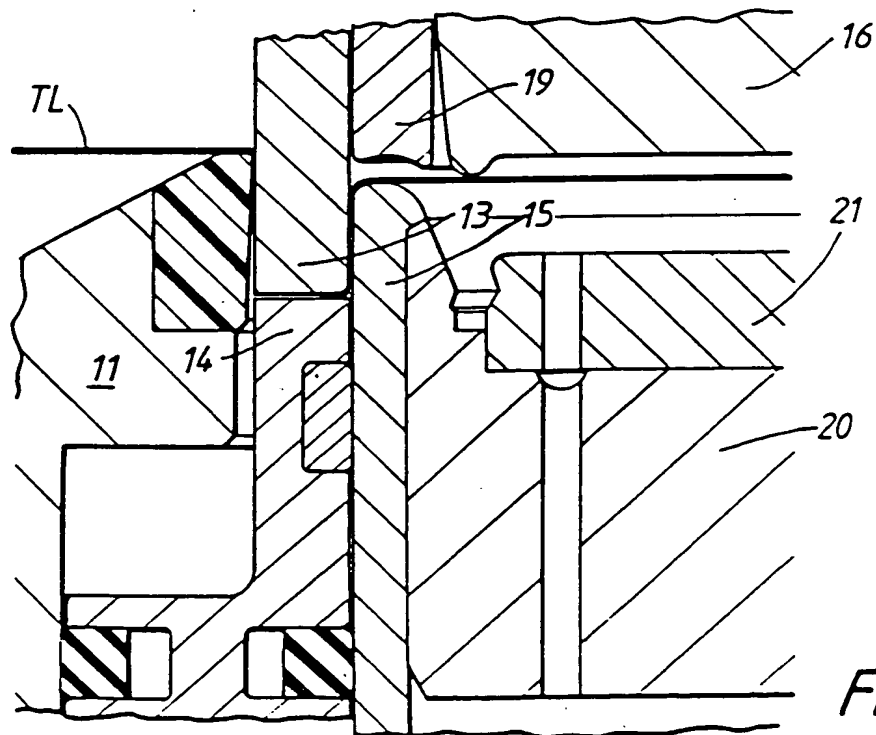
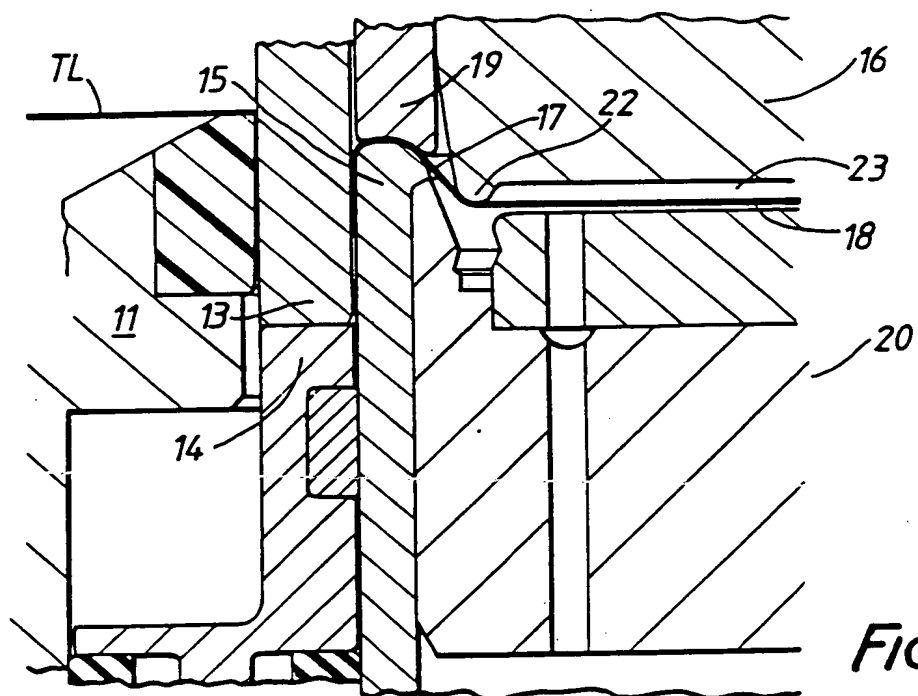
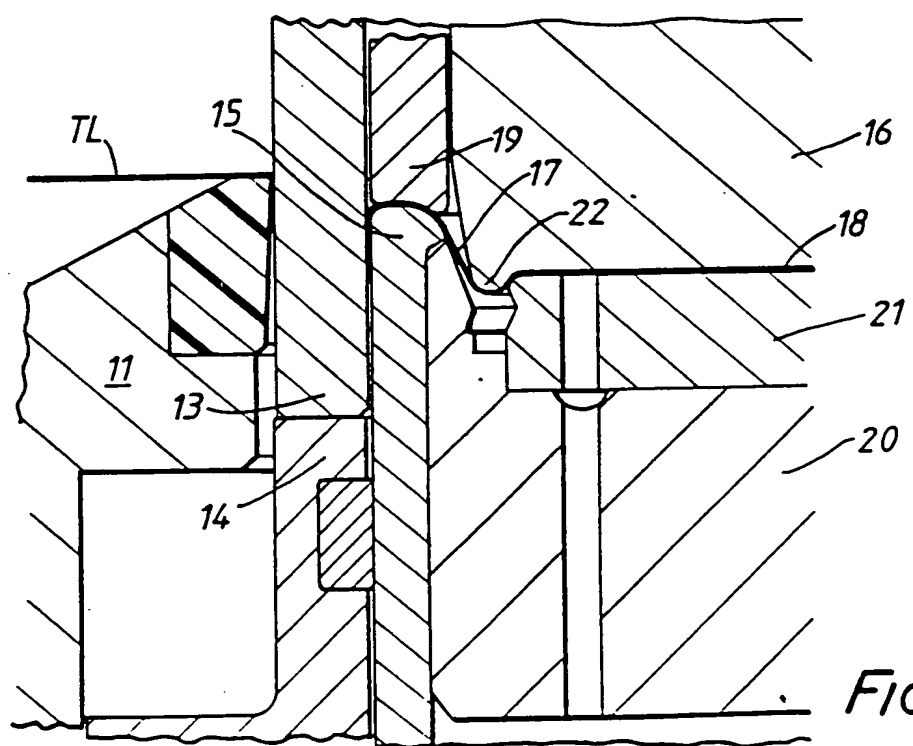


FIG. 2.



**FIG. 3.**



**FIG. 4.**

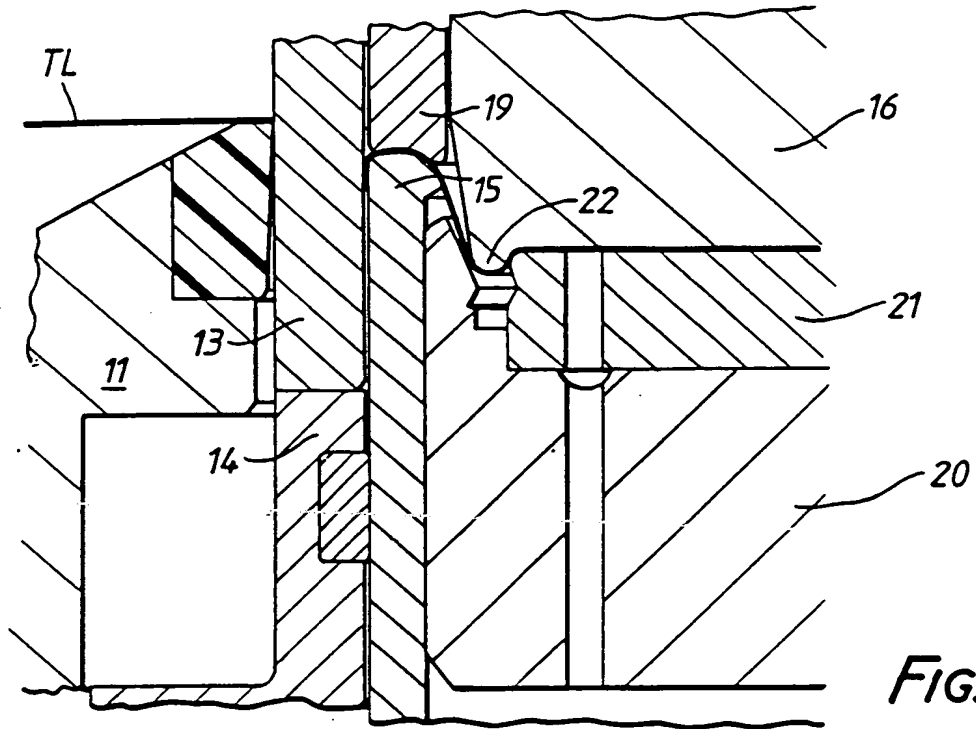


FIG. 5.

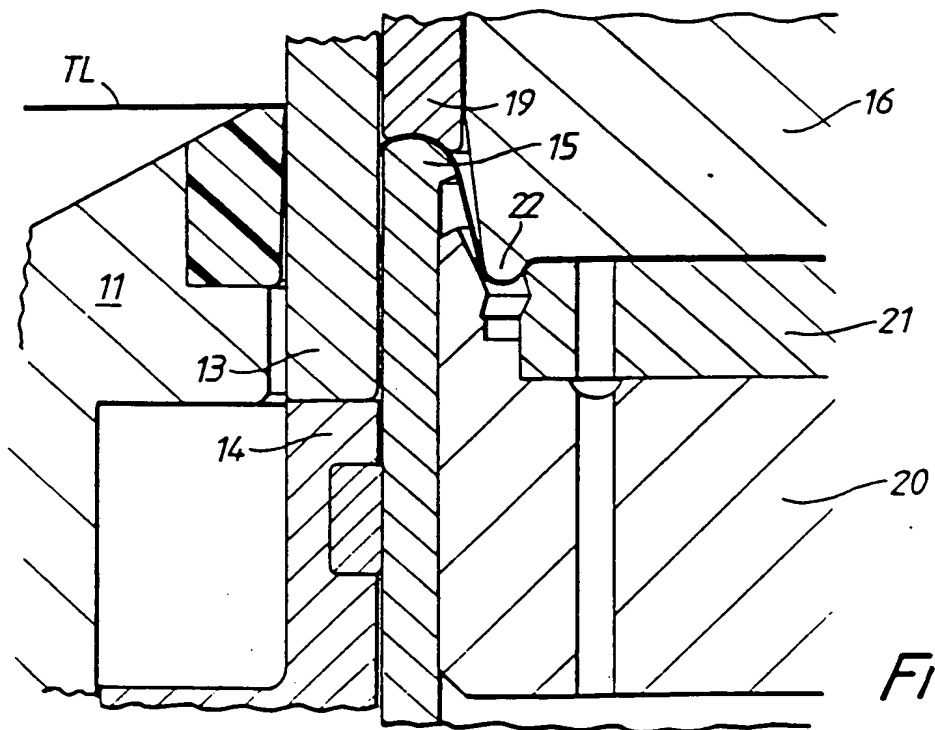


FIG. 6.

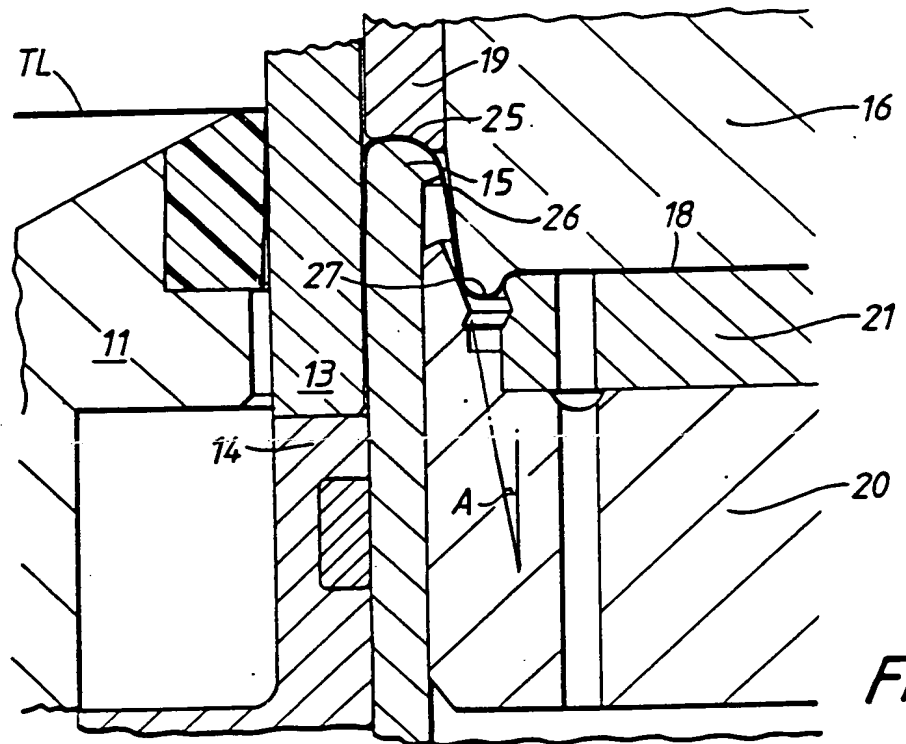


FIG. 7

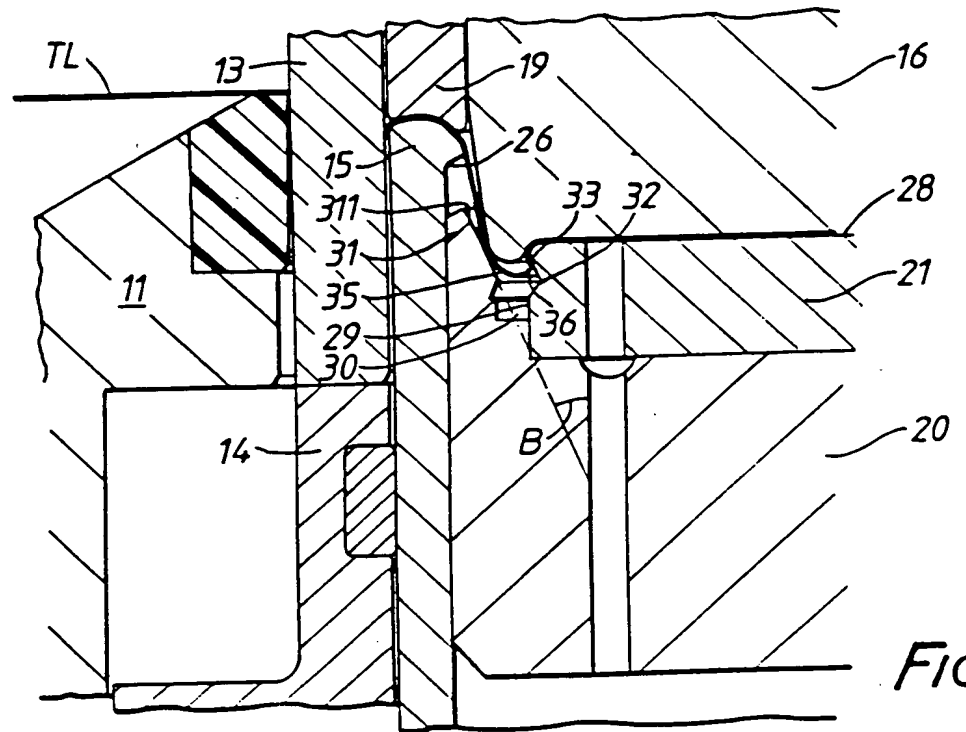
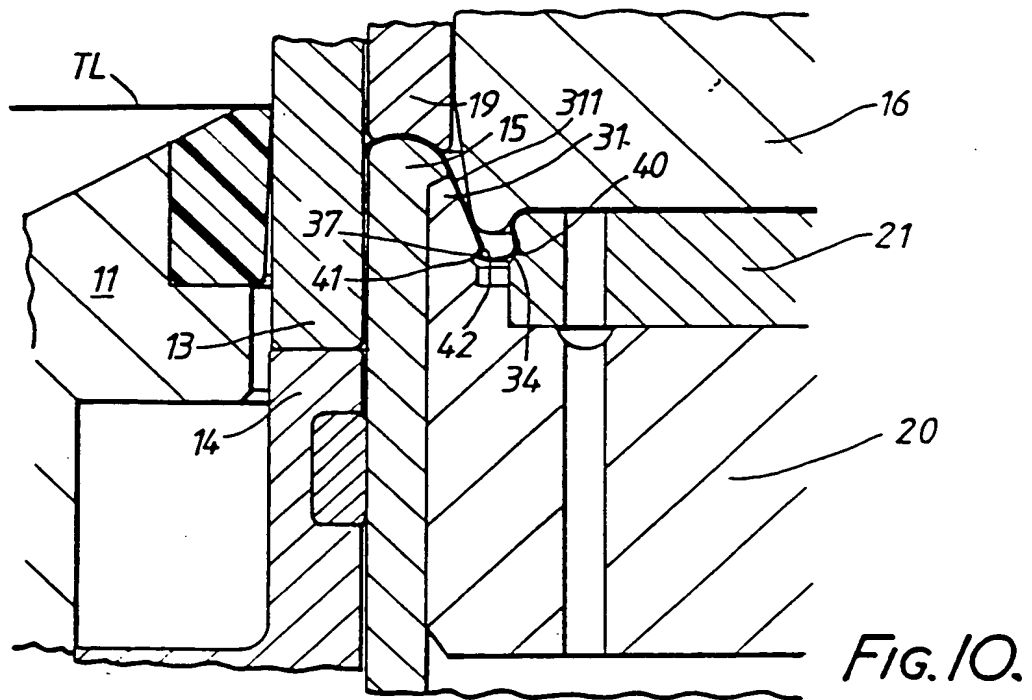
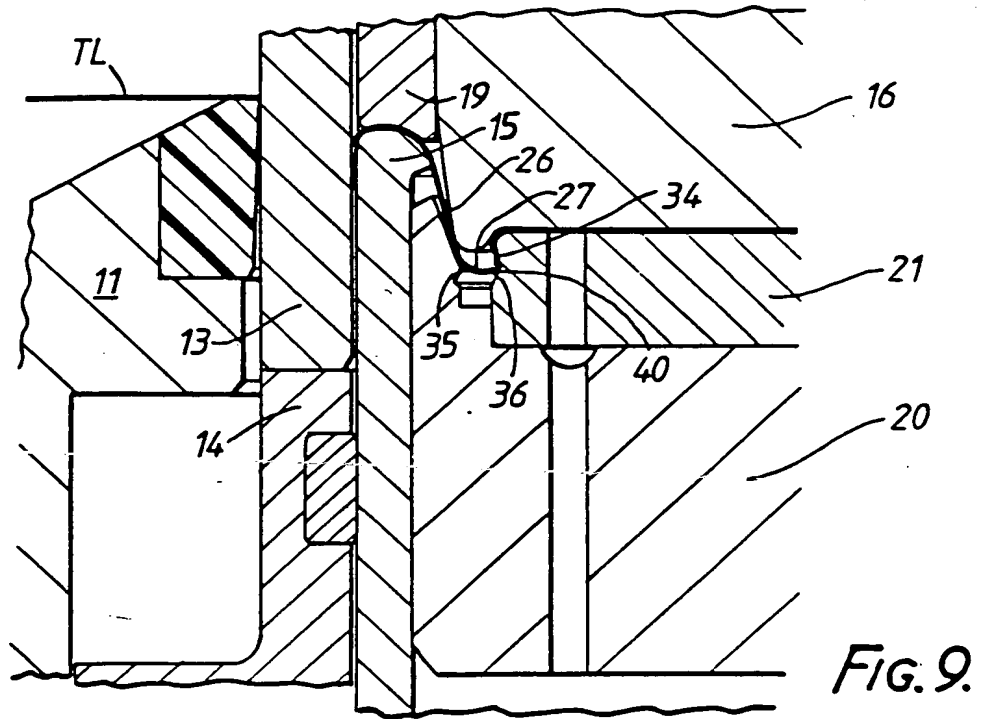
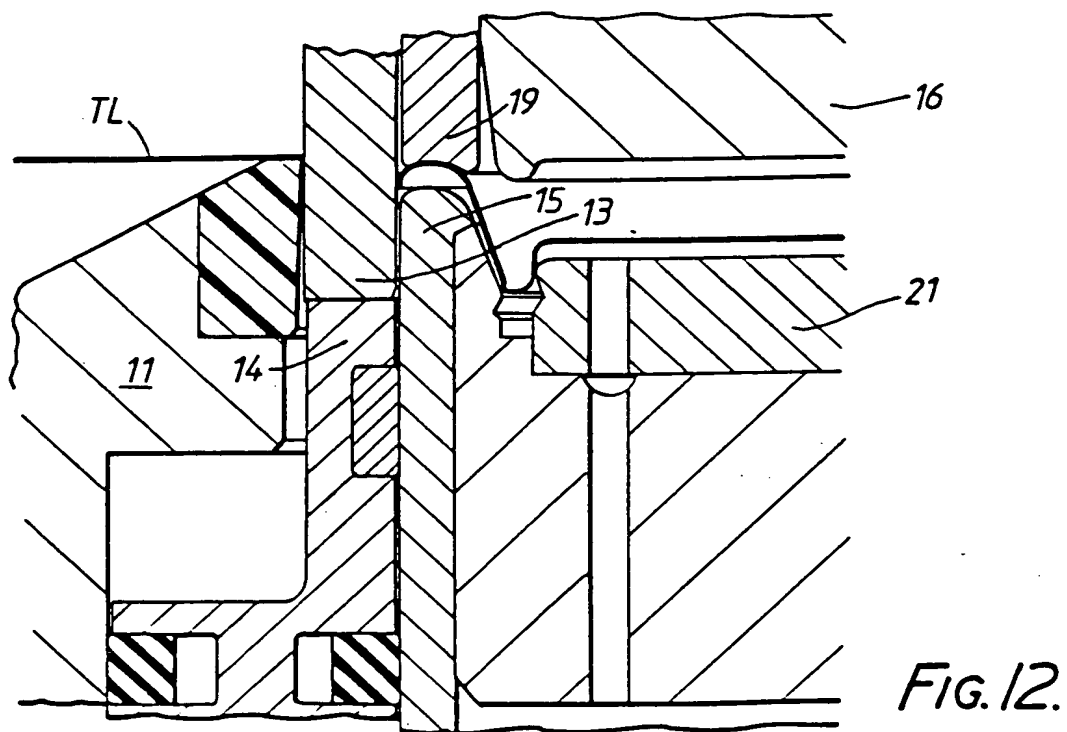
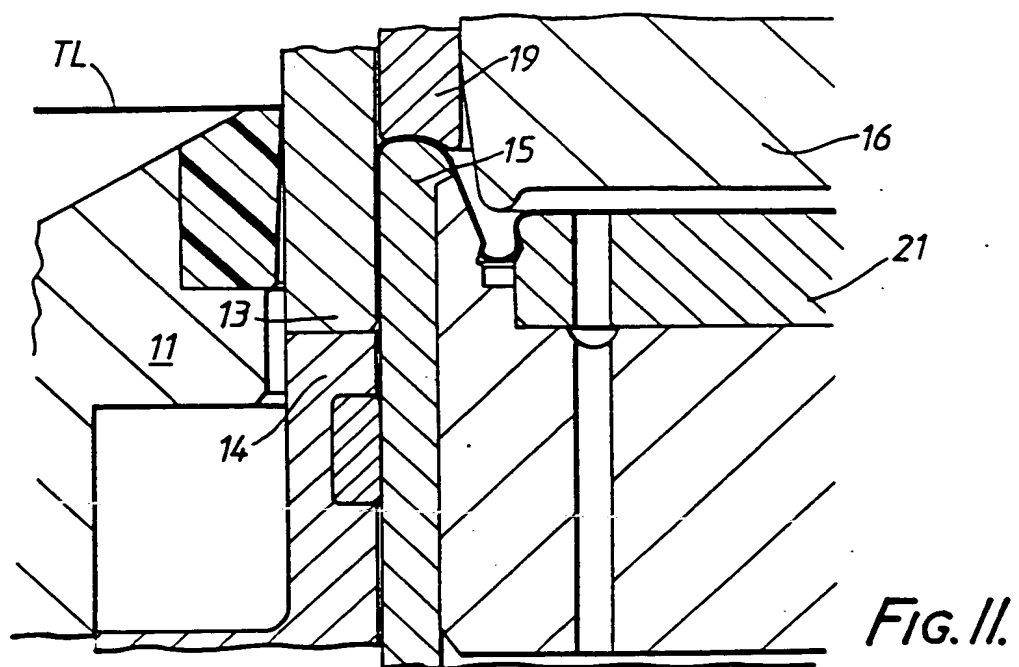
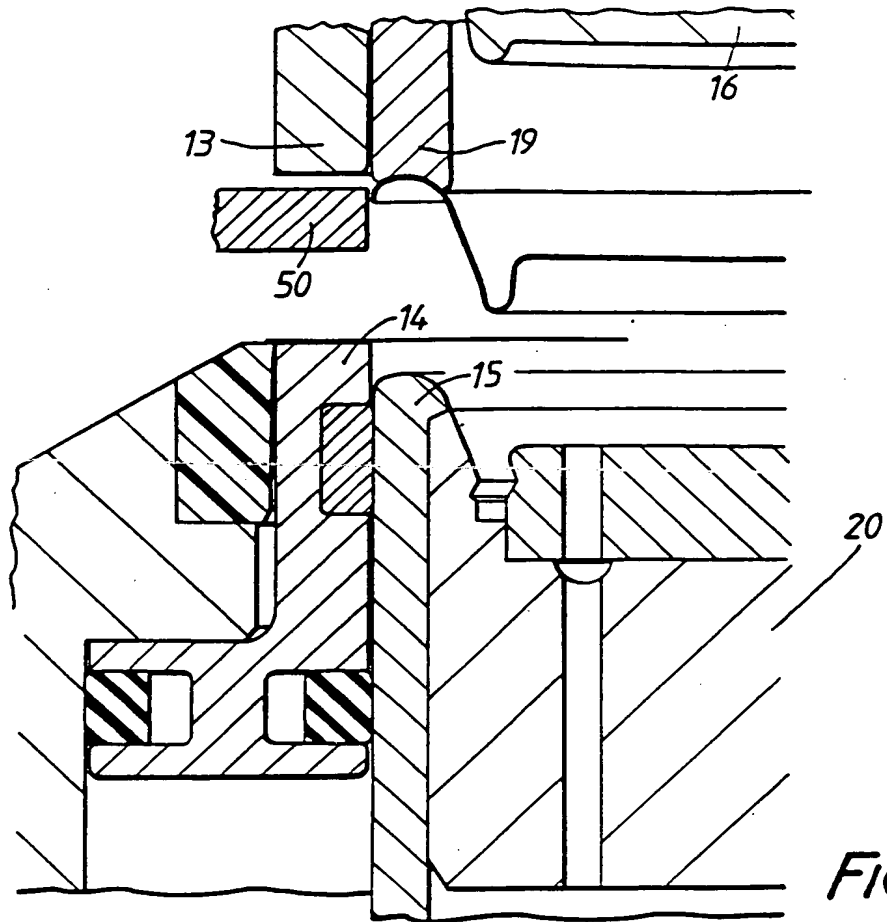


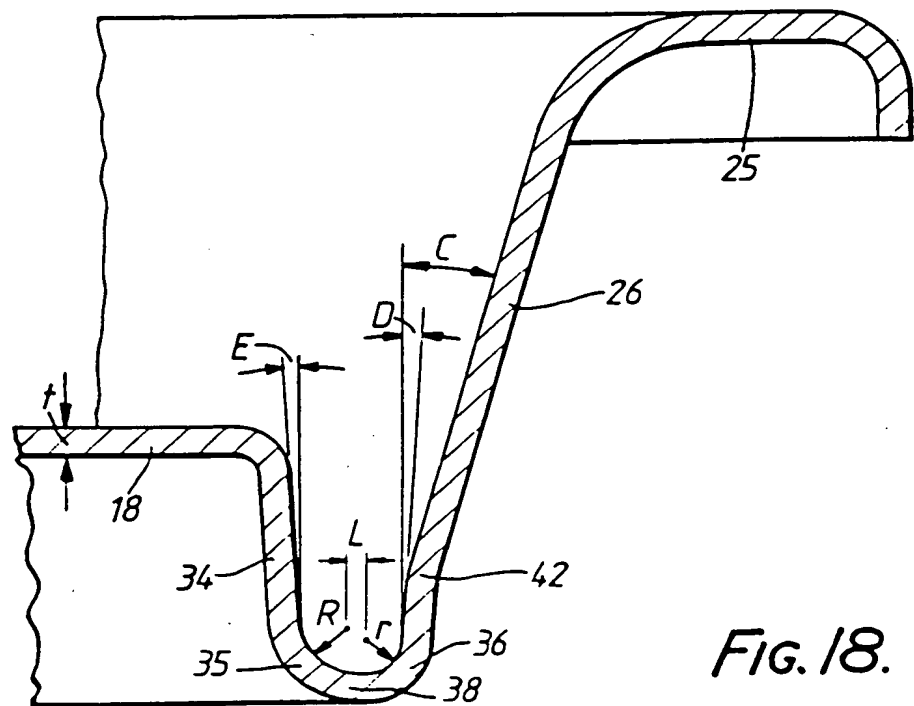
FIG. 8.







*FIG. 13.*



*FIG. 18.*

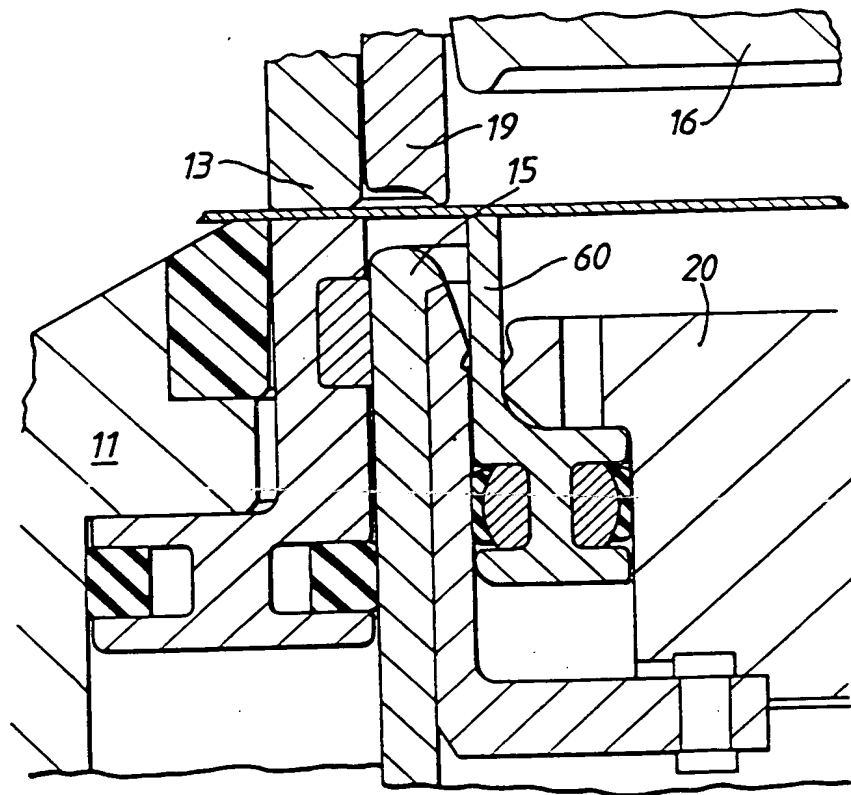


FIG. 14.

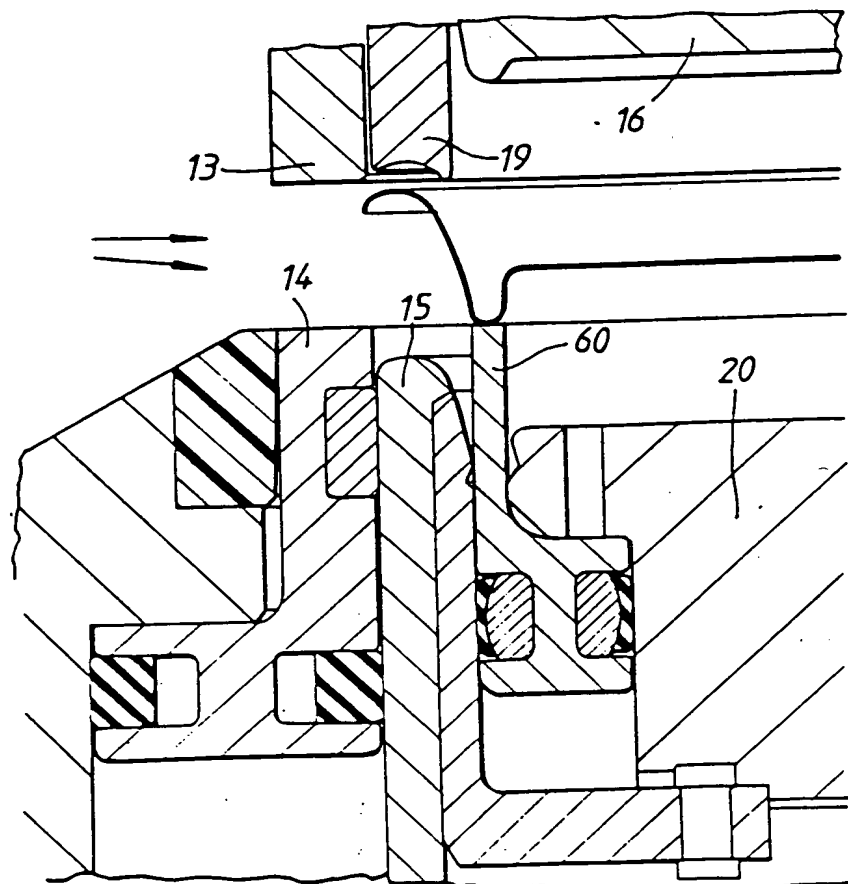


FIG. 15.



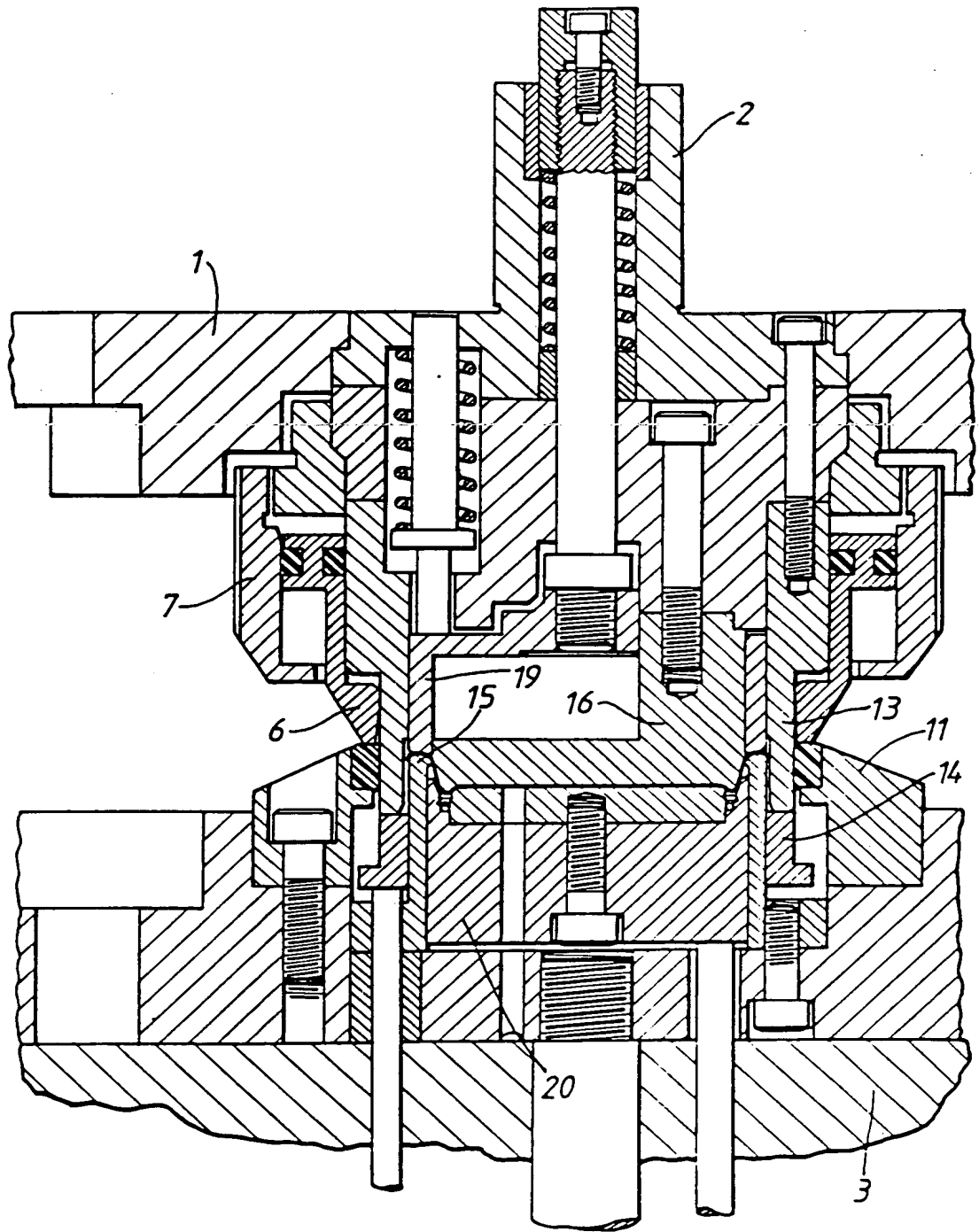


FIG. 16.

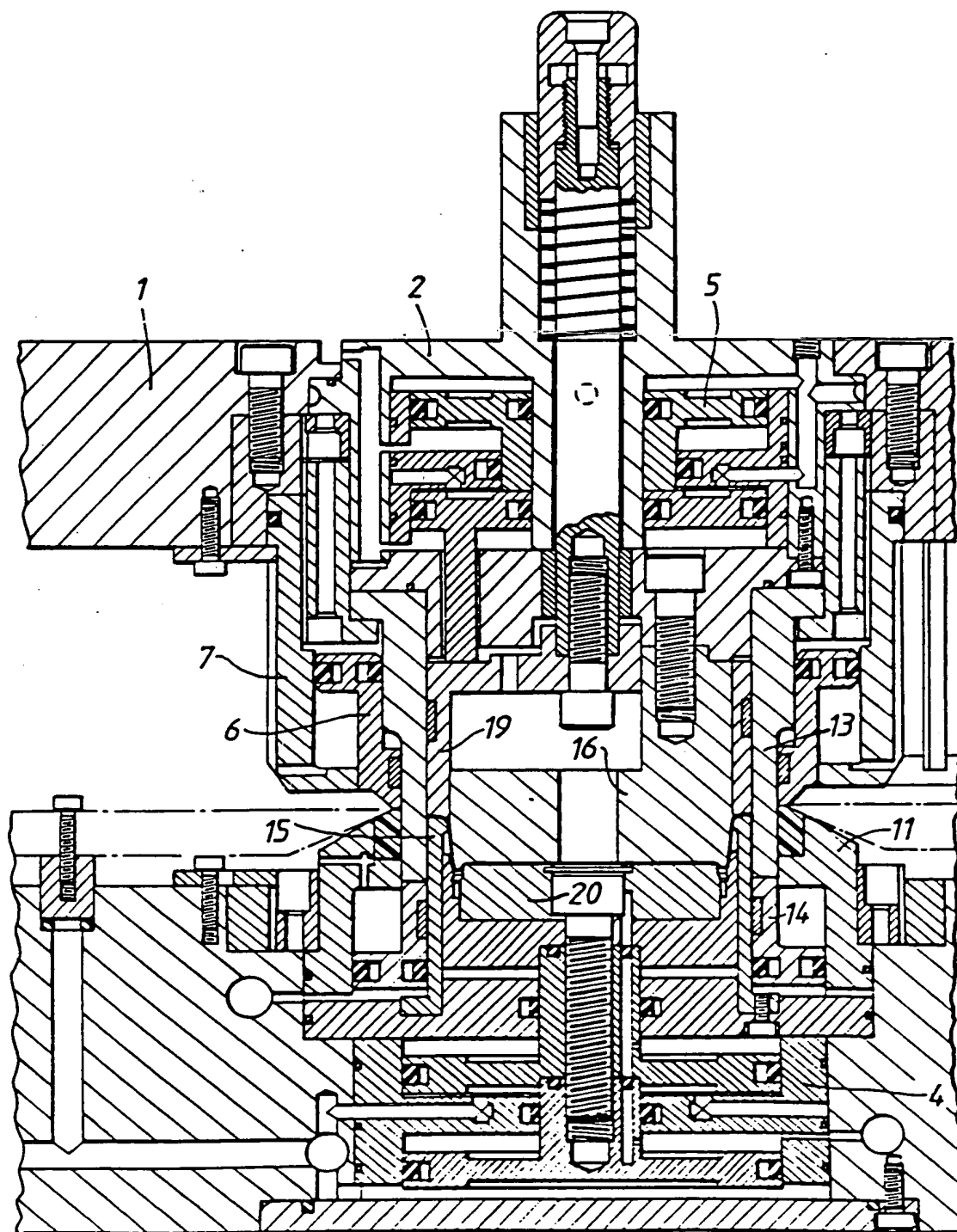


FIG. 17

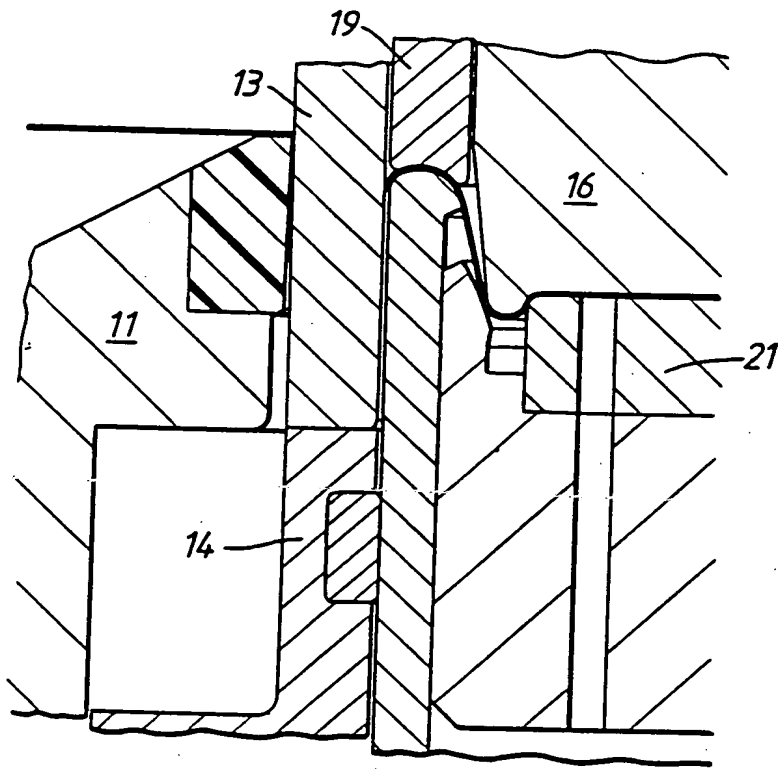


FIG. 19.

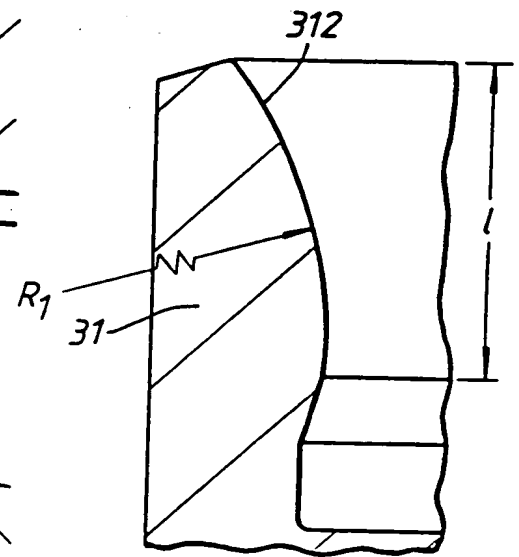


FIG. 20.

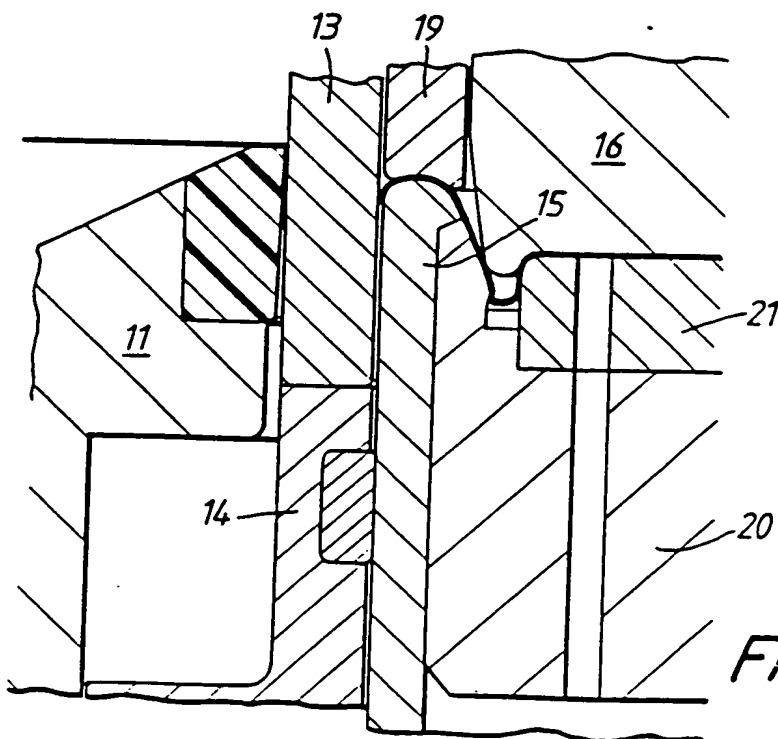


FIG. 21.



European Patent  
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# EUROPEAN SEARCH REPORT

Application Number

EP 89 30 4071

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 4)
X	GB-A-2 067 159 (WILKINSON) * Whole document *	6, 7, 10	B 21 D 51/38 B 65 D 7/36
X	US-A-4 574 608 (REDICON CORP.) * Column 6, lines 39-73; columns 7, 8; figures *	1, 4, 5, 8, 9	
D, A	EP-A-0 153 115 (METAL BOX)		
D, A	US-A-3 537 291 (REYNOLDS METALS CO.)		
D, A	US-A-4 109 599 (ALUMINUM CO.)		
A	US-A-4 031 837 (ALUMINUM CO.)		
A	US-A-4 716 755 (REDICON CORP.)		
A	US-A-4 713 958 (REDICON CORP.)		
A	US-A-4 715 208 (REDICON CORP.)		
A	EP-A-0 139 282 (BALL CORP.)		
The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (Int. Cl. 4)
			B 21 D B 65 D
Place of search THE HAGUE		Date of completion of the search 28-07-1989	Examiner PEETERS L.
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X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons ..... & : member of the same patent family, corresponding document	